## Voltage Drop Calculations For Engineers - Beginners

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## Voltage drop formulas //

Voltage drop calculations using the DC-resistance formula are not always accurate for AC circuits, especially for those with a less-than-unity power factor or for those that use conductors larger than 2 AWG.

Table 1 allows engineers to perform simple ac voltage drop calculations. Table 1 was compiled using the NeherMcGrath ac-resistance calculation method, and the values presented are both reliable and conservative. This table contains completed calculations of effective impedance ( $Z$ ) for the average ac circuit with an 85 percent power factor (see Calculation Example 1).

If calculations with a different power factor are necessary, Table 1 also contains the appropriate values of inductive reactance and AC resistance (see Example 2).

## The basic assumptions and the limitations of Table 1 are as follows:

1. Capacitive reactance is ignored.
2. There are three conductors in a raceway.
3. The calculated voltage drop values are approximate.
4. For circuits with other parameters, the Neher-McGrath ac-resistance calculation method is used.

## Calculation Example \#1

A feeder has a 100 A continuous load. The system source is 240 volts, 3 phase, and the supplying circuit breaker is 125 A. The feeder is in a trade size $11 / 4$ aluminum conduit with three 1 AWG THHN copper conductors operating at their maximum temperature rating of $75^{\circ} \mathrm{C}$. The circuit length is $\mathbf{1 5 0} \mathbf{f t}$, and the power factor is $\mathbf{8 5}$ percent.

Using Table 1 below, determine the approximate voltage drop of this circuit.

## See the solution //

STEP-1 // Find the approximate line-to-neutral voltage drop.
Using the Table 1 column "Effective Zat 0.85 PF for Uncoated Copper Wires", select aluminum conduit and size 1 AWG copper wire. Use the given value of 0.16 ohm per 1000 ft in the following formula:

$$
\begin{aligned}
\text { Voltage drop }_{(\text {line-l-o-neutral }} & =\begin{array}{c}
\text { table } \\
\text { value }
\end{array} \frac{\begin{array}{c}
\text { circuit } \\
\text { length }
\end{array}}{1000 \mathrm{ft}} \times{ }_{\text {load }}^{\text {circuit }}
\end{aligned}
$$

STEP-2 // Find the line-to-line voltage drop:

$$
\begin{aligned}
\text { Voltage }^{\text {drop }}{ }_{(\text {line-to-line) }} & =\text { voltage drop } \\
& =2.40 \mathrm{~V} \times 1.732 \\
& =4.157 \mathrm{~V}
\end{aligned}
$$

STEP-3 // Find the voltage present at the load end of the circuit:

$$
240 \mathrm{~V}-4.157 \mathrm{~V}=235.84 \mathrm{~V}
$$

## Calculation Example \#2

A 270 A continuous load is present on a feeder. The circuit consists of a single 4-in. PVC conduit with three 600kcmil XHHW/USE aluminum conductors fed from a 480 V , 3-phase, 3-wire source. The conductors are operating at their maximum rated temperature of $75^{\circ} \mathrm{C}$.

If the power factor is $\mathbf{0 . 7}$ and the circuit length is $\mathbf{2 5 0} \mathbf{f t}$, is the voltage drop excessive?

## See the solution //

STEP-1 I/ Using the Table 1 column " $X_{L}$ (Reactance) for All Wires", select PVC conduit and the row for size $\mathbf{6 0 0} \mathbf{k c m i l}$ A value of $\mathbf{0 . 0 3 9}$ ohm per 1000 ft is given as this $\mathbf{X}_{\mathrm{L}}$. Next, using the column "Alternating-Current Resistance for Aluminum Wires", select PVC conduit and the row for size 600 kcmil . A value of $\mathbf{0 . 0 3 6}$ ohm per $\mathbf{1 0 0 0} \mathbf{f t}$ is given as this R.

STEP-2 // Find the angle representing a power factor of 0.7.

Using a calculator with trigonometric functions or a trigonometric function table, find the arccosine $\left(\cos ^{-1}\right) \theta$ of 0.7 , which is 45.57 degrees. For this example, call this angle.

STEP-3 // Find the impedance $(\mathbf{Z})$ corrected to 0.7 power factor $\left(\mathbf{Z}_{\mathbf{c}}\right)$ :
STEP-4 // As in Calculation Example 1, find the approximate line-toneutral voltage drop:

$$
\begin{aligned}
Z_{c} & =(R \times \cos \theta)+\left(X_{L} \times \sin \theta\right) \\
& =(0.036 \times 0.7)+(0.039 \times 0.7141) \\
& =0.0252+0.0279 \\
& =0.0531 \text { ohm to neutral }
\end{aligned}
$$

$$
\begin{aligned}
\text { Voltage drop }_{(\text {line-to-neural) }} & =Z_{c} \times \frac{\text { circuit length }}{1000 \mathrm{ft}} \times \text { circuit load } \\
& =0.0531 \times \frac{250 \mathrm{ft}}{1000 \mathrm{ft}} \times 270 \mathrm{~A} \\
& =3.584 \mathrm{~V}
\end{aligned}
$$

STEP-5 // Find the approximate line-to-line voltage drop:
STEP-6 // Find the approximate voltage drop expressed as a percentage of the circuit voltage:

STEP-7 // Find the voltage present at the load end of the circuit:

$$
\begin{aligned}
\text { Voltage drop }_{(\text {line-t-l-line) }} & =\text { voltage drop } \\
& =3.584 \mathrm{~V} \times 1.732 \\
& =6.208 \mathrm{~V}
\end{aligned}
$$

Conclusion // According to 210.19(A)(1), Informational Note No. 4, this voltage drop does not appear to be excessive.

$$
\begin{aligned}
\text { Percentage voltage drop }_{\text {(line-l-a-line) }} & =\frac{6.208 \mathrm{~V}}{480 \mathrm{~V}} \times 100 \\
& =1.29 \% \mathrm{VD}
\end{aligned}
$$

## TABLE 1 //

$$
480 \mathrm{~V}-6.208 \mathrm{~V}=473.8 \mathrm{~V}
$$

## Alternating-Current Resistance and Reactance for 600-Volt Cables, 3-Phase, $60 \mathrm{~Hz}, 75^{\circ} \mathrm{C}\left(167^{\circ} \mathrm{F}\right)$

## Three Single Conductors in Conduit //

| $\begin{gathered} \text { Size } \\ \text { (AWG } \\ \text { or } \\ \text { kcmil) } \end{gathered}$ | $\frac{\text { Ohms to Neutral per Kilometer }}{\text { Ohms to Neutral per } 1000 \text { Feet }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|c} \text { Size } \\ \text { (AWG } \\ \text { or } \\ \text { kcmil) } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $X_{L}$ (Reactance) <br> for All Wires |  | Alternating-Current Resistance for Uncoated Copper Wires |  |  | Alternating-Current Resistance for Aluminum Wires |  |  | Effective Z at 0.85 PF for Uncoated Copper Wires |  |  | Effective Z at 0.85 PF for Aluminum Wires |  |  |  |
|  | $\begin{array}{\|c\|} \hline \text { PVC, } \\ \text { Alumi- } \\ \text { num } \\ \text { Conduits } \end{array}$ | Steel <br> Conduit | PVC <br> Conduit | $\begin{aligned} & \text { Alumi- } \\ & \text { num } \\ & \text { Conduit } \end{aligned}$ | Steel Conduit | PVC Conduit | $\begin{array}{\|c\|} \text { Alumi- } \\ \text { num } \\ \text { Conduit } \end{array}$ | Steel <br> Conduit | PVC Conduit | $\begin{array}{\|c\|} \text { Alumi- } \\ \text { num } \\ \text { Conduit } \end{array}$ | Steel Conduit | PVC <br> Conduit | Aluminum Conduit | Steel Conduit |  |
| 14 | $\begin{aligned} & 0.190 \\ & 0.058 \end{aligned}$ | $\begin{aligned} & 0.240 \\ & 0.073 \end{aligned}$ | $\begin{array}{r} 10.2 \\ 3.1 \\ \hline \end{array}$ | $\begin{array}{r} 10.2 \\ 3.1 \\ \hline \end{array}$ | $\begin{array}{r} 10.2 \\ 3.1 \\ \hline \end{array}$ | - | - | - | $\begin{aligned} & 8.9 \\ & 2.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8.9 \\ & 2.7 \end{aligned}$ | $\begin{aligned} & 8.9 \\ & 2.7 \end{aligned}$ | - | - | - | 14 |
| 12 | $\begin{aligned} & 0.177 \\ & 0.054 \end{aligned}$ | $\begin{aligned} & 0.223 \\ & 0.068 \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} 10.5 \\ 3.2 \\ \hline \end{array}$ | $\begin{array}{r} 10.5 \\ 3.2 \\ \hline \end{array}$ | $\begin{array}{r} 10.5 \\ 3.2 \\ \hline \end{array}$ | $\begin{aligned} & 5.6 \\ & 1.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.6 \\ & 1.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.6 \\ & 1.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.2 \\ & 2.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.2 \\ & 2.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.2 \\ & 2.8 \end{aligned}$ | 12 |
| 10 | $\begin{aligned} & 0.164 \\ & 0.050 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.207 \\ & 0.063 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.9 \\ & 1.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.9 \\ & 1.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.9 \\ & 1.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.6 \\ & 1.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.6 \\ & 1.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.6 \\ & 1.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.9 \\ & 1.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.9 \\ & 1.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.9 \\ & 1.8 \\ & \hline \end{aligned}$ | 10 |
| 8 | $\begin{aligned} & 0.171 \\ & 0.052 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.213 \\ & 0.065 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.56 \\ & 0.78 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.56 \\ & 0.78 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.56 \\ & 0.78 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.3 \\ & 1.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.3 \\ & 1.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.3 \\ & 1.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.26 \\ & 0.69 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.26 \\ & 0.69 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.30 \\ & 0.70 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.6 \\ & 1.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.6 \\ & 1.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.6 \\ & 1.1 \\ & \hline \end{aligned}$ | 8 |
| 6 | $\begin{aligned} & 0.167 \\ & 0.051 \end{aligned}$ | $\begin{aligned} & 0.210 \\ & 0.064 \end{aligned}$ | $\begin{aligned} & 1.61 \\ & 0.49 \end{aligned}$ | $\begin{aligned} & 1.61 \\ & 0.49 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.61 \\ & 0.49 \end{aligned}$ | $\begin{aligned} & 2.66 \\ & 0.81 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.66 \\ & 0.81 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.66 \\ & 0.81 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.44 \\ & 0.44 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.48 \\ & 0.45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.48 \\ & 0.45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.33 \\ & 0.71 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.36 \\ & 0.72 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.36 \\ & 0.72 \\ & \hline \end{aligned}$ | 6 |
| 4 | $\begin{aligned} & 0.157 \\ & 0.048 \end{aligned}$ | $\begin{aligned} & 0.197 \\ & 0.060 \end{aligned}$ | $\begin{aligned} & 1.02 \\ & 0.31 \end{aligned}$ | $\begin{aligned} & 1.02 \\ & 0.31 \end{aligned}$ | $\begin{aligned} & 1.02 \\ & 0.31 \end{aligned}$ | $\begin{aligned} & 1.67 \\ & 0.51 \end{aligned}$ | $\begin{aligned} & 1.67 \\ & 0.51 \end{aligned}$ | $\begin{aligned} & 1.67 \\ & 0.51 \end{aligned}$ | $\begin{aligned} & 0.95 \\ & 0.29 \end{aligned}$ | $\begin{aligned} & 0.95 \\ & 0.29 \end{aligned}$ | $\begin{aligned} & 0.98 \\ & 0.30 \end{aligned}$ | $\begin{aligned} & 1.51 \\ & 0.46 \end{aligned}$ | $\begin{aligned} & 1.51 \\ & 0.46 \end{aligned}$ | $\begin{aligned} & 1.51 \\ & 0.46 \end{aligned}$ | 4 |
| 3 | $\begin{aligned} & 0.154 \\ & 0.047 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.194 \\ & 0.059 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.25 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.25 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.25 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.31 \\ & 0.40 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.35 \\ & 0.41 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.31 \\ & 0.40 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.75 \\ & 0.23 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.79 \\ & 0.24 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.79 \\ & 0.24 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.21 \\ & 0.37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.21 \\ & 0.37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.21 \\ & 0.37 \\ & \hline \end{aligned}$ | 3 |
| 2 | $\begin{aligned} & 0.148 \\ & 0.045 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.187 \\ & 0.057 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.62 \\ & 0.19 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.05 \\ & 0.32 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.05 \\ & 0.32 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.05 \\ & 0.32 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.62 \\ & 0.19 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.62 \\ & 0.19 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.98 \\ & 0.30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.98 \\ & 0.30 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.98 \\ & 0.30 \\ & \hline \end{aligned}$ | 2 |
| 1 | $\begin{aligned} & 0.151 \\ & 0.046 \end{aligned}$ | $\begin{aligned} & 0.187 \\ & 0.057 \end{aligned}$ | $\begin{aligned} & 0.49 \\ & 0.15 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & 0.85 \\ & 0.26 \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.79 \\ & 0.24 \end{aligned}$ | $\begin{aligned} & 0.79 \\ & 0.24 \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.25 \end{aligned}$ | 1 |
| 1/0 | $\begin{aligned} & 0.144 \\ & 0.044 \end{aligned}$ | $\begin{aligned} & 0.180 \\ & 0.055 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 0.12 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 0.12 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.69 \\ & 0.21 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.62 \\ & 0.19 \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.20 \\ & \hline \end{aligned}$ | $1 / 0$ |
| $2 / 0$ | $\begin{aligned} & 0.141 \\ & 0.043 \end{aligned}$ | $\begin{aligned} & 0.177 \\ & 0.054 \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.16 \end{aligned}$ | $2 / 0$ |
| 3/0 | $\begin{aligned} & 0.138 \\ & 0.042 \end{aligned}$ | $\begin{aligned} & 0.171 \\ & 0.052 \end{aligned}$ | $\begin{aligned} & 0.253 \\ & 0.077 \end{aligned}$ | $\begin{aligned} & 0.269 \\ & 0.082 \end{aligned}$ | $\begin{aligned} & 0.259 \\ & 0.079 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.289 \\ & 0.088 \end{aligned}$ | $\begin{aligned} & 0.302 \\ & 0.092 \end{aligned}$ | $\begin{aligned} & 0.308 \\ & 0.094 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.46 \\ & 0.14 \end{aligned}$ | 3/0 |
| 4/0 | $\begin{aligned} & 0.135 \\ & 0.041 \end{aligned}$ | $\begin{aligned} & 0.167 \\ & 0.051 \end{aligned}$ | $\begin{aligned} & 0.203 \\ & 0.062 \end{aligned}$ | $\begin{aligned} & 0.220 \\ & 0.067 \end{aligned}$ | $\begin{aligned} & 0.207 \\ & 0.063 \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.243 \\ & 0.074 \end{aligned}$ | $\begin{aligned} & 0.256 \\ & 0.078 \end{aligned}$ | $\begin{aligned} & 0.262 \\ & 0.080 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.11 \end{aligned}$ | 4/0 |
| 250 | $\begin{aligned} & 0.135 \\ & 0.041 \end{aligned}$ | $\begin{aligned} & 0.171 \\ & 0.052 \end{aligned}$ | $\begin{aligned} & 0.171 \\ & 0.052 \end{aligned}$ | $\begin{aligned} & 0.187 \\ & 0.057 \end{aligned}$ | $\begin{aligned} & 0.177 \\ & 0.054 \end{aligned}$ | $\begin{aligned} & 0.279 \\ & 0.085 \end{aligned}$ | $\begin{aligned} & 0.295 \\ & 0.090 \end{aligned}$ | $\begin{aligned} & 0.282 \\ & 0.086 \end{aligned}$ | $\begin{aligned} & 0.217 \\ & 0.066 \end{aligned}$ | $\begin{aligned} & 0.230 \\ & 0.070 \end{aligned}$ | $\begin{aligned} & 0.240 \\ & 0.073 \end{aligned}$ | $\begin{aligned} & 0.308 \\ & 0.094 \end{aligned}$ | $\begin{aligned} & 0.322 \\ & 0.098 \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.10 \end{aligned}$ | 250 |
| 300 | $\begin{aligned} & 0.135 \\ & 0.041 \end{aligned}$ | $\begin{aligned} & 0.167 \\ & 0.051 \end{aligned}$ | $\begin{aligned} & 0.144 \\ & 0.044 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.161 \\ & 0.049 \end{aligned}$ | $\begin{aligned} & 0.148 \\ & 0.045 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.233 \\ & 0.071 \end{aligned}$ | $\begin{aligned} & 0.249 \\ & 0.076 \end{aligned}$ | $\begin{aligned} & 0.236 \\ & 0.072 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.194 \\ & 0.059 \end{aligned}$ | $\begin{aligned} & 0.207 \\ & 0.063 \end{aligned}$ | $\begin{aligned} & 0.213 \\ & 0.065 \end{aligned}$ | $\begin{aligned} & 0.269 \\ & 0.082 \end{aligned}$ | $\begin{aligned} & 0.282 \\ & 0.086 \end{aligned}$ | $\begin{aligned} & 0.289 \\ & 0.088 \end{aligned}$ | 300 |
| 350 | $\begin{aligned} & 0.131 \\ & 0.040 \end{aligned}$ | $\begin{aligned} & 0.164 \\ & 0.050 \end{aligned}$ | $\begin{aligned} & 0.125 \\ & 0.038 \end{aligned}$ | $\begin{aligned} & 0.141 \\ & 0.043 \end{aligned}$ | $\begin{aligned} & 0.128 \\ & 0.039 \end{aligned}$ | $\begin{aligned} & 0.200 \\ & 0.061 \end{aligned}$ | $\begin{aligned} & 0.217 \\ & 0.066 \end{aligned}$ | $\begin{aligned} & 0.207 \\ & 0.063 \end{aligned}$ | $\begin{aligned} & 0.174 \\ & 0.053 \end{aligned}$ | $\begin{aligned} & 0.190 \\ & 0.058 \end{aligned}$ | $\begin{aligned} & 0.197 \\ & 0.060 \end{aligned}$ | $\begin{aligned} & 0.240 \\ & 0.073 \end{aligned}$ | $\begin{aligned} & 0.253 \\ & 0.077 \end{aligned}$ | $\begin{aligned} & 0.262 \\ & 0.080 \end{aligned}$ | 350 |
| 400 | $\begin{aligned} & 0.131 \\ & 0.040 \end{aligned}$ | $\begin{aligned} & 0.161 \\ & 0.049 \end{aligned}$ | $\begin{aligned} & 0.108 \\ & 0.033 \end{aligned}$ | $\begin{aligned} & 0.125 \\ & 0.038 \end{aligned}$ | $\begin{aligned} & 0.115 \\ & 0.035 \end{aligned}$ | $\begin{aligned} & 0.177 \\ & 0.054 \end{aligned}$ | $\begin{aligned} & 0.194 \\ & 0.059 \end{aligned}$ | $\begin{aligned} & 0.180 \\ & 0.055 \end{aligned}$ | $\begin{aligned} & 0.161 \\ & 0.049 \end{aligned}$ | $\begin{aligned} & 0.174 \\ & 0.053 \end{aligned}$ | $\begin{aligned} & 0.184 \\ & 0.056 \end{aligned}$ | $\begin{aligned} & 0.217 \\ & 0.066 \end{aligned}$ | $\begin{aligned} & 0.233 \\ & 0.071 \end{aligned}$ | $\begin{aligned} & 0.240 \\ & 0.073 \end{aligned}$ | 400 |
| 500 | $\begin{aligned} & 0.128 \\ & 0.039 \end{aligned}$ | $\begin{aligned} & 0.157 \\ & 0.048 \end{aligned}$ | $\begin{aligned} & 0.089 \\ & 0.027 \end{aligned}$ | $\begin{aligned} & 0.105 \\ & 0.032 \end{aligned}$ | $\begin{aligned} & 0.095 \\ & 0.029 \end{aligned}$ | $\begin{aligned} & 0.141 \\ & 0.043 \end{aligned}$ | $\begin{aligned} & 0.157 \\ & 0.048 \end{aligned}$ | $\begin{aligned} & 0.148 \\ & 0.045 \end{aligned}$ | $\begin{aligned} & 0.141 \\ & 0.043 \end{aligned}$ | $\begin{aligned} & 0.157 \\ & 0.048 \end{aligned}$ | $\begin{aligned} & 0.164 \\ & 0.050 \end{aligned}$ | $\begin{aligned} & 0.187 \\ & 0.057 \end{aligned}$ | $\begin{aligned} & 0.200 \\ & 0.061 \end{aligned}$ | $\begin{aligned} & 0.210 \\ & 0.064 \end{aligned}$ | 500 |
| 600 | $\begin{aligned} & 0.128 \\ & 0.039 \end{aligned}$ | $\begin{aligned} & 0.157 \\ & 0.048 \end{aligned}$ | $\begin{aligned} & 0.075 \\ & 0.023 \end{aligned}$ | $\begin{aligned} & 0.092 \\ & 0.028 \end{aligned}$ | $\begin{aligned} & 0.082 \\ & 0.025 \end{aligned}$ | $\begin{aligned} & 0.118 \\ & 0.036 \end{aligned}$ | $\begin{aligned} & 0.135 \\ & 0.041 \end{aligned}$ | $\begin{aligned} & 0.125 \\ & 0.038 \end{aligned}$ | $\begin{aligned} & 0.131 \\ & 0.040 \end{aligned}$ | 0.144 0.044 | $\begin{aligned} & 0.154 \\ & 0.047 \end{aligned}$ | $\begin{aligned} & 0.167 \\ & 0.051 \end{aligned}$ | $\begin{aligned} & 0.180 \\ & 0.055 \end{aligned}$ | $\begin{aligned} & 0.190 \\ & 0.058 \end{aligned}$ | 600 |
| 750 | $\begin{aligned} & 0.125 \\ & 0.038 \end{aligned}$ | $\begin{aligned} & 0.157 \\ & 0.048 \end{aligned}$ | $\begin{aligned} & 0.062 \\ & 0.019 \end{aligned}$ | $\begin{aligned} & 0.079 \\ & 0.024 \end{aligned}$ | $\begin{aligned} & 0.069 \\ & 0.021 \end{aligned}$ | $\begin{aligned} & 0.095 \\ & 0.029 \end{aligned}$ | $\begin{aligned} & 0.112 \\ & 0.034 \end{aligned}$ | $\begin{aligned} & 0.102 \\ & 0.031 \end{aligned}$ | $\begin{aligned} & 0.118 \\ & 0.036 \end{aligned}$ | $\begin{aligned} & 0.131 \\ & 0.040 \end{aligned}$ | $\begin{aligned} & 0.141 \\ & 0.043 \end{aligned}$ | $\begin{aligned} & 0.148 \\ & 0.045 \end{aligned}$ | $\begin{aligned} & 0.161 \\ & 0.049 \end{aligned}$ | $\begin{aligned} & 0.171 \\ & 0.052 \end{aligned}$ | 750 |
| 1000 | $\begin{aligned} & 0.121 \\ & 0.037 \end{aligned}$ | $\begin{aligned} & 0.151 \\ & 0.046 \end{aligned}$ | $\begin{aligned} & 0.049 \\ & 0.015 \end{aligned}$ | $\begin{aligned} & 0.062 \\ & 0.019 \end{aligned}$ | $\begin{aligned} & 0.059 \\ & 0.018 \end{aligned}$ | $\begin{aligned} & 0.075 \\ & 0.023 \end{aligned}$ | $\begin{aligned} & 0.089 \\ & 0.027 \end{aligned}$ | $\begin{aligned} & 0.082 \\ & 0.025 \end{aligned}$ | $\begin{aligned} & 0.105 \\ & 0.032 \end{aligned}$ | $\begin{aligned} & 0.118 \\ & 0.036 \end{aligned}$ | $\begin{aligned} & 0.131 \\ & 0.040 \end{aligned}$ | $\begin{aligned} & 0.128 \\ & 0.039 \end{aligned}$ | $\begin{aligned} & 0.138 \\ & 0.042 \end{aligned}$ | $\begin{aligned} & 0.151 \\ & 0.046 \end{aligned}$ | 1000 |

TABLE 1 - Alternating-Current Resistance and Reactance for 600-Volt Cables, 3-Phase, $60 \mathrm{~Hz}, 75^{\circ} \mathrm{C}\left(167^{\circ} \mathrm{F}\right)$ - Three Single Conductors in Conduit

Reference // National Electrical Code Handbook - Mark W. Earley, P.E., Jeffrey S. Sargent, Christopher D. Coache and Richard J. Roux (National Fire Protection Association, Quincy, Massachusetts)

